

17th Annual Design and Installation of Cost-Efficient Piles Conference



Charleston Marriott, Charleston, South Carolina Wednesday, September 21 and Thursday, September 22, 2016



Innovative Solution for

Marine Fenders
Foundations
2.

Seawall Structures

Kevin Lathan, PEConstruction e Link, Inc.

&

V. Larry Tsimmerman, PE

Omega Trestle, LLC



FLANGED PIPE PILE

(FPP)

a NEW TOOL

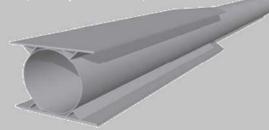
for your driven pile solutions

Toolbox.





New structural section The OMEGA Section



Omega Beam when horizontal

&

Flanged Pipe Pile (FPP) when driven

FPP section is built up from fundamental shapes

Advantages:

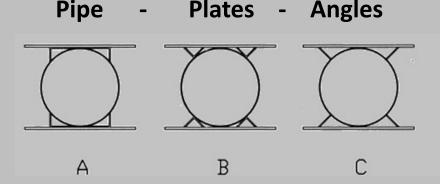
Available
Scalable to any size
Economical

Fabricate anywhere

High STRONG to SECONDARY axis ratio of about 2:1

Greater bending strength & smaller footprint than pipe of equal weight

Significant increase in torsional, and asymmetrical loading capacity





FPP as driven pile solution

For: LOAD CASES

Lateral loads - piers, wharfs and fenders

Earth Retention- connected & lagged systems



FPP as driven pile solution

When: GEOMETRICALLY CONSTRAINED

- Anchoring piles into ROCK strata
- Minimized footprint desired
- No space for battered pile lateral restraint

First, a little background on the Omega Project

Omega Project Background



TESTING



MANUFACTURING



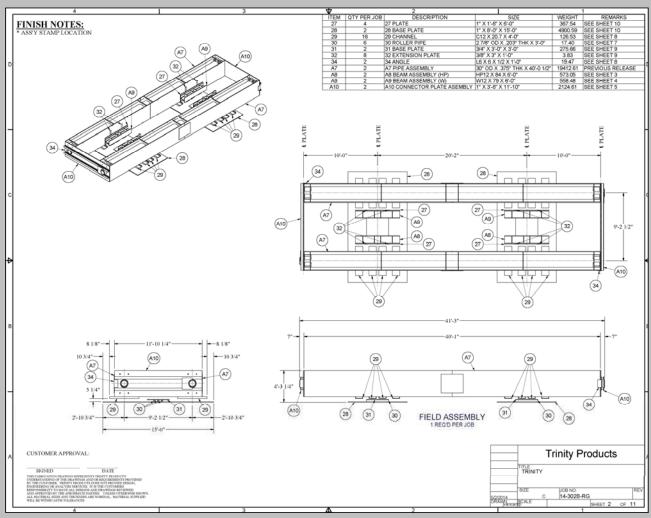
FIELD DEPLOYMENT

TESTING TEST 1

Maximum Bending Moment

Maximum Shear & Full shear end connection test







Two (2) 800 Ton Jacks Certified and Calibrated

Application of jack forces and instrumentation was in general accordance with ASTM 1143/D 1143M-07 and adapted for this horizontal application.

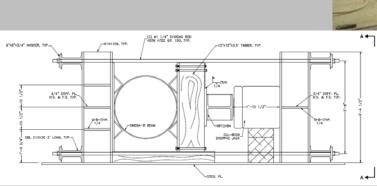
TESTING

Proof Load 275 Tons

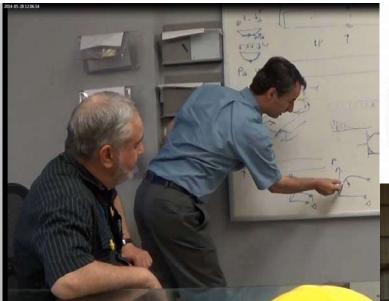
TEST 2

Compression Test

Localized "Crush Test"







Special thanks to:

The Ohio State University & Dr. Halil Sezen, P.E. Professor of Civil Engineering

Dr. Sezen provided his valuable assistance with the static load tests on the Omega Beams in St. Charles MO in May & June 2014.

We look forward to continuing our knowledge sharing relationship with The Ohio State University and Dr. Sezen.



MANUFACTURING

Nearly 3,000 LF of beams moved into production in late 2014







MANUFACTURING







FIELD DEPLOYMENT -

Pre-assembly & Barge Transport

1,200 LF of Trestle = 30 Spans at 40 ft. for a 300 Ton Manitowoc 2250 Crane – Baltimore, MD



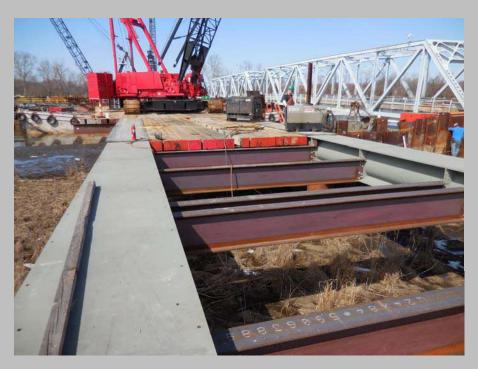
Frame style trestle in 40 ft. sections

Span by span loaded to barge

FIELD DEPLOYMENT

Span by span installation, MD, Eastern Shore





FIELD DEPLOYMENT

Span by span installation, MD, Eastern Shore





PDCA Charleston, SC

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FIELD DEPLOYMENT

Span by span installation & production pile starts



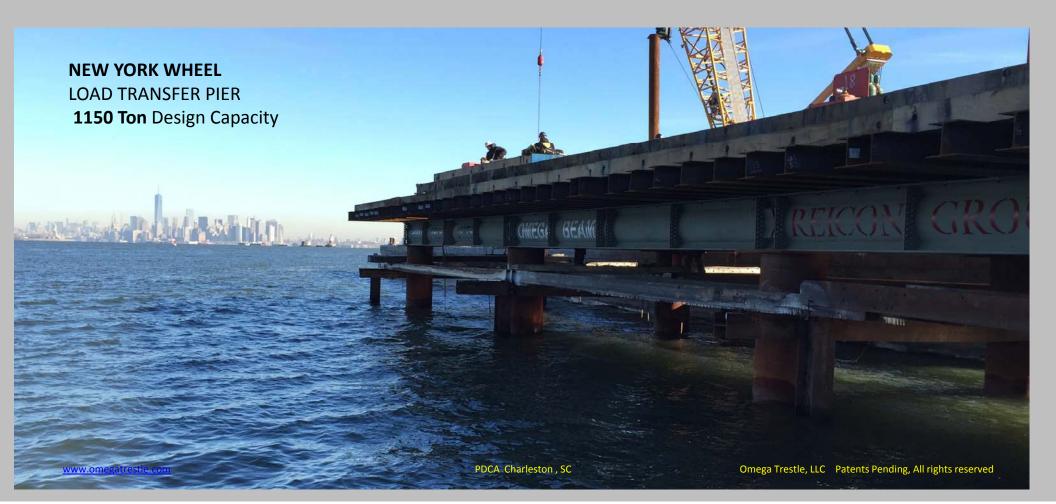




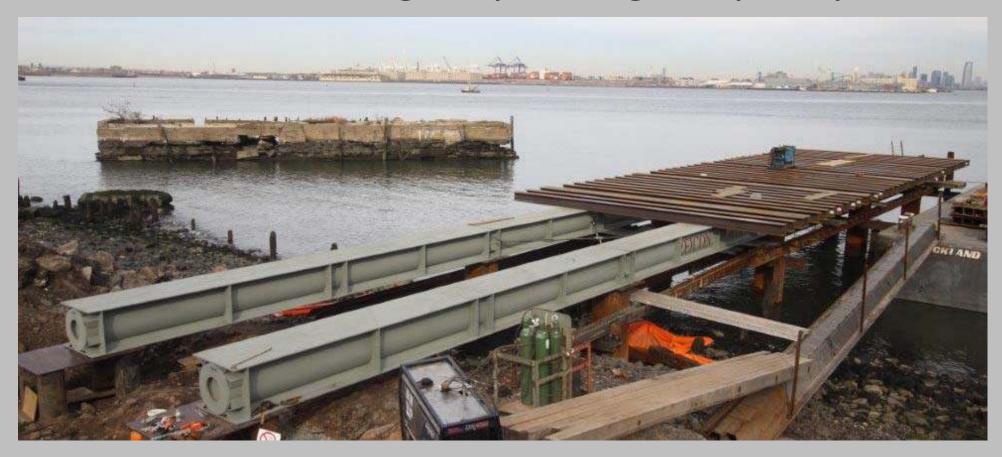
Omega Trestle in Service in girder erection



Another application: as High Capacity Pier



E Elevated Omega Style - High Capacity Pier



E Elevated Omega Style - High Capacity Pier some details

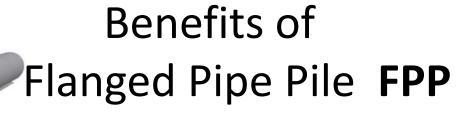




NY WHEEL - High Capacity Pier







Marine Fenders

C

Foundations



FPP as part of driven pile toolbox for :

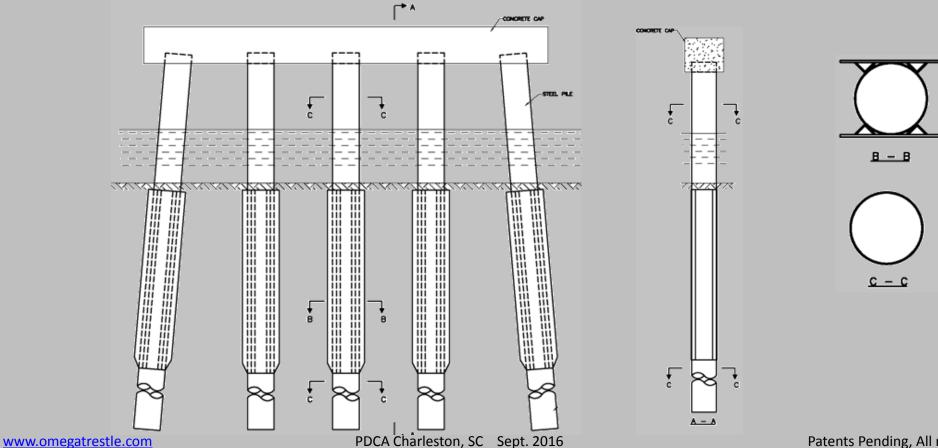
Lateral loads cases

I. Cyclical such as Current, wind, & seismic

II. Impact- collision bollards or marine fender

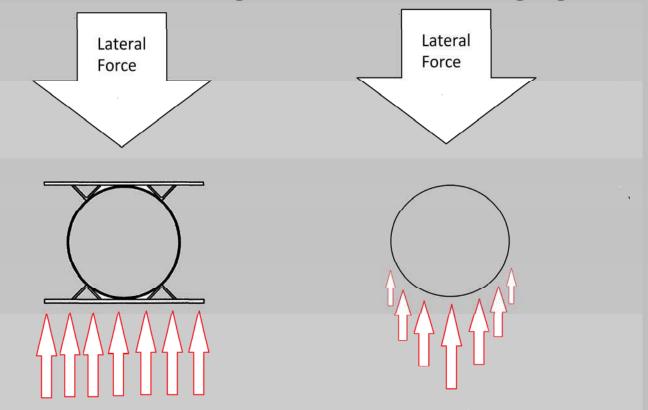
Pier Example 1:

Improve performance in poor soils by increasing bending capacity, surface area and radius of gyration



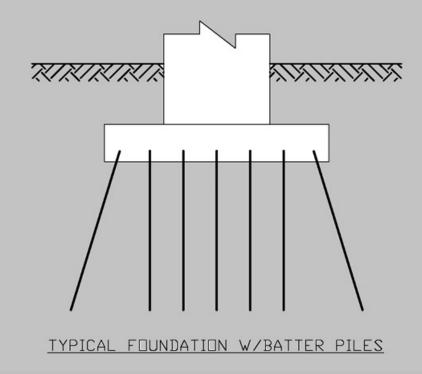
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Improved lateral geotechnical engagement

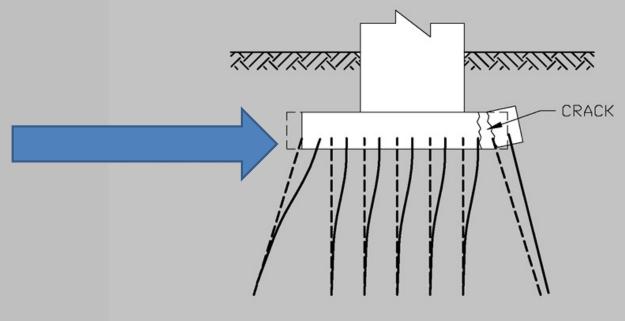


Geotechnical reactive forces shown in above schematics are approximated to highlight benefits of FPP geometry

Pier Example 2: Typical bridge pier with batter piles used for lateral load resistance

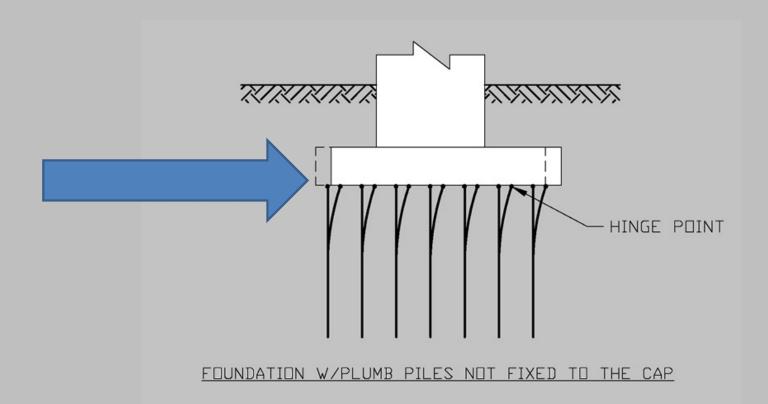


Batter pile foundations are effective, <u>but</u> can cause substantial damage when subjected to seismic, wind or impact loading due to lateral stiffness



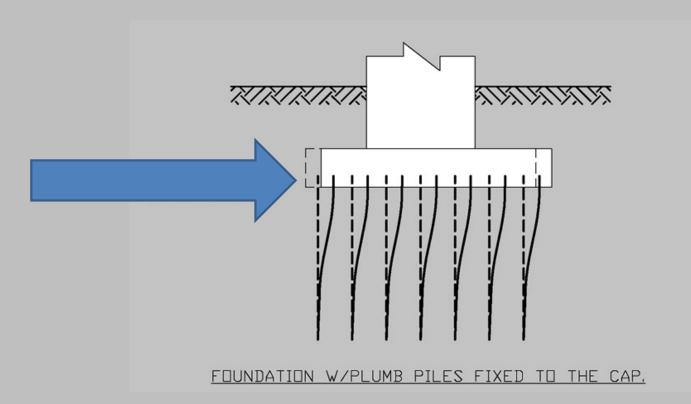
TYPICAL DAMAGE IN FOUNDATION W/BATTER PILES

Plumb pile foundations are not as stiff as the foundations with batter piles. Such foundations absorb energy better during lateral loading events.





Plumb pile foundation with fixed connection to the pile cap.





When we select a steel pile for a foundation, our options are;

1. Pipe

- optimized to resist <u>compression</u> and <u>torsion</u>.

$$Sy/Sx = 1$$

- -often less economical when it comes to <u>bending</u> because it has extra material around neutral axis area.
- 2. H-pile
- limited in size when hot rolled.
- much weaker in one direction than the other.

$$Sy/Sx=0.30 +/-$$

3. FPP a new piling option to consider ...

The FPP

Fundamentals of effectiveness

60-70 % Stronger than H-pile in weak direction.

Unique section at

$$Sy/Sx = 0.50 + /-$$

Greater crushing strength than pipe alone!

- Angles and plates reinforce pipe section.
- Pipe compression and bending capacity is improved significantly
- Addition of flanges can improve performance of any pipe section
- Very stable section due to use of pipe as "web"
- Scalable ability to use the flanges only where needed in the vertical column





FPP as part of driven pile toolbox for :

Geometric constraints

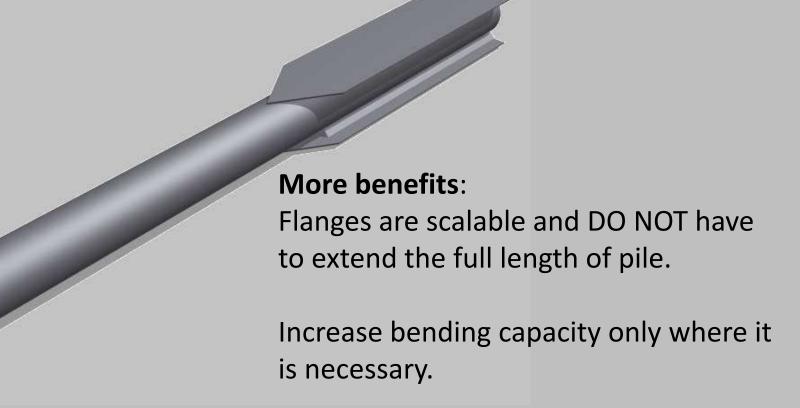
I. When more compact section is preferred

a. fender system where no room available for batter pile

b. wharf retrofit with permit constraints

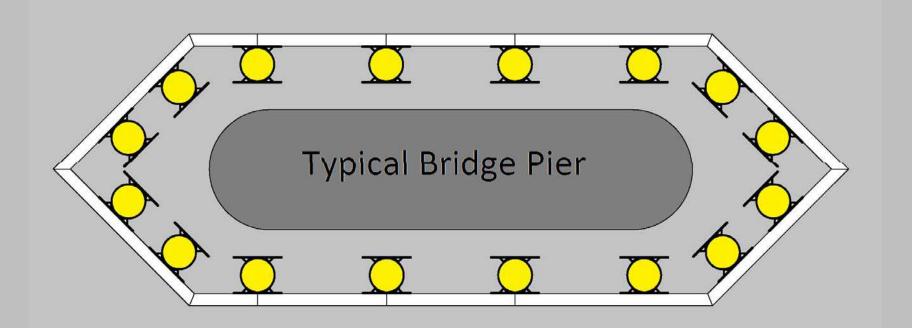
II. When anchoring into rock strata is required pipe better than W or H section FPP is has additional benefits

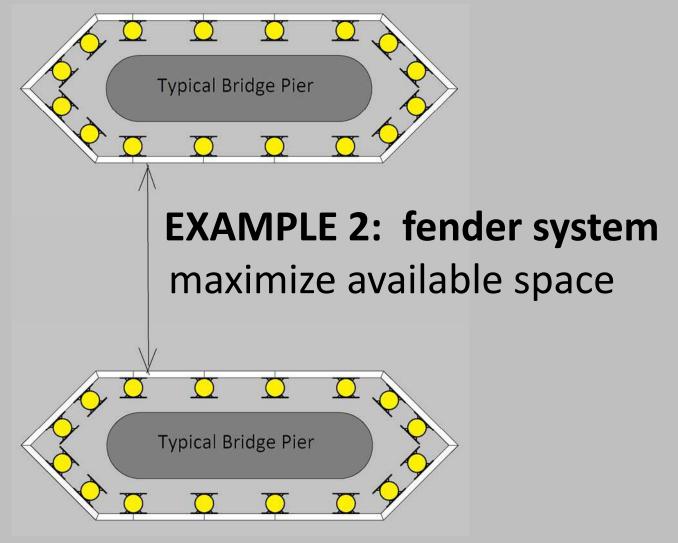
Flanged Pipe Pile (FPP)



compact section for lateral load resistance EXAMPLE: fender

where batter piles are not possible





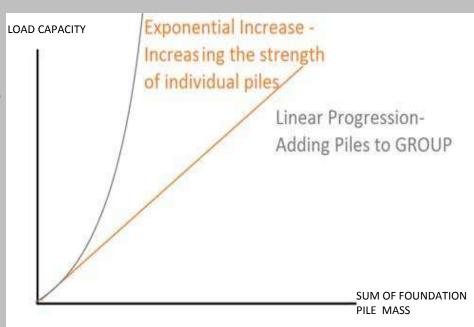
Individual Piles vs. Pile Group

GIVEN: Piles act as individual piles in granular soils if their spacing is greater than 7 times the pile diameter;

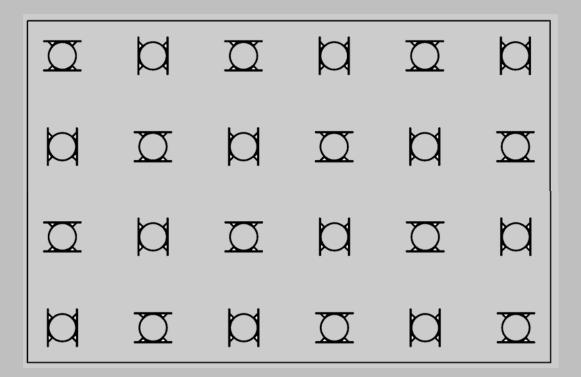
GIVEN: Bearing capacity of pile groups is generally less than the sum of individual piles.

THEN, in order to increase capacity of the foundation you need to increase strength of piles without significant increase of their dimensions.

SOLUTION: Consider utilizing a FLANGED PIPE PILE (FPP) This is what it does!



Because of smaller dimensions more FPP's can fit within the same foundation footprint than pipe piles.

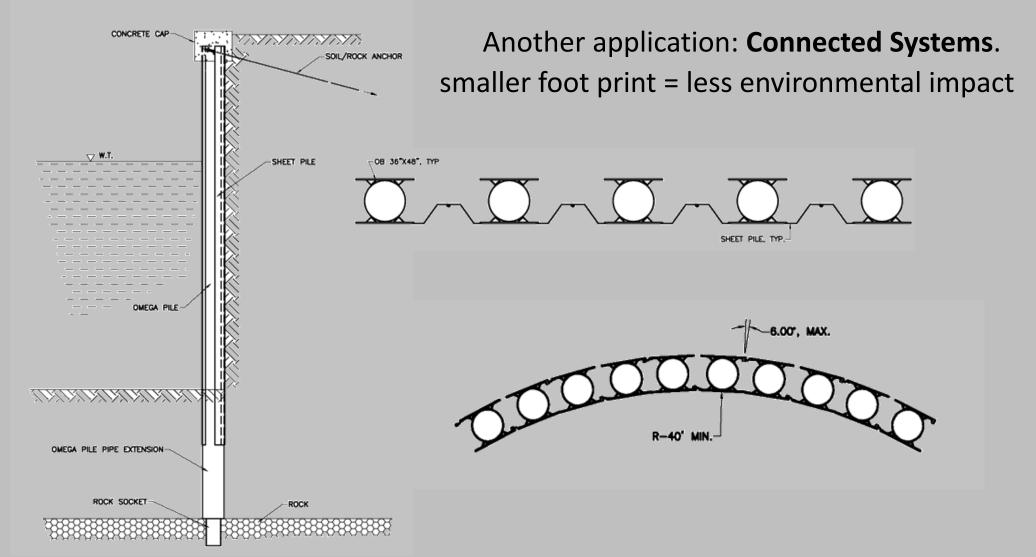


Greater Sy/Sx ratio allows to achieve greater resistance to horizontal loads than that of H-pile foundations. Hollow tubular core provides opportunity to break up obstructions and to anchor piles to rock.





Seawalls & connected systems

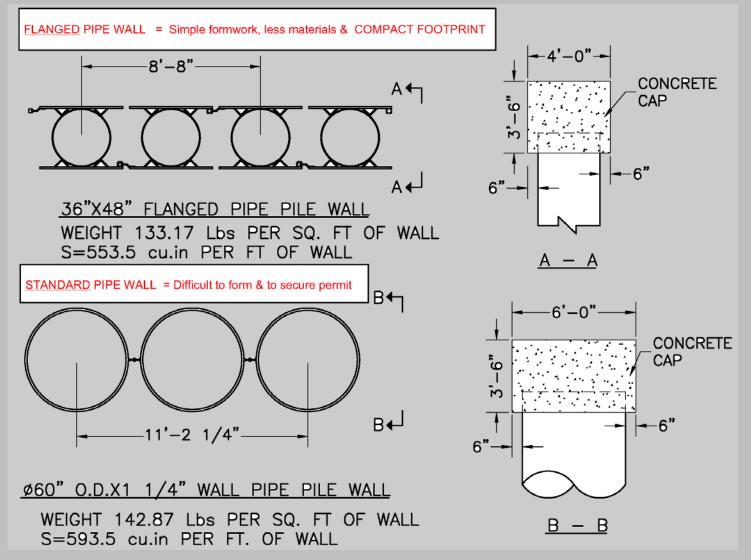


PIPE Wall

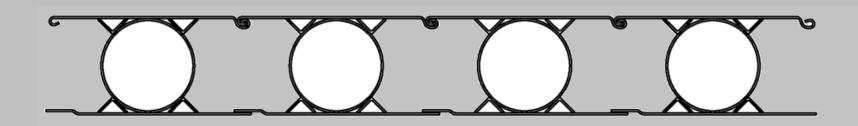
or

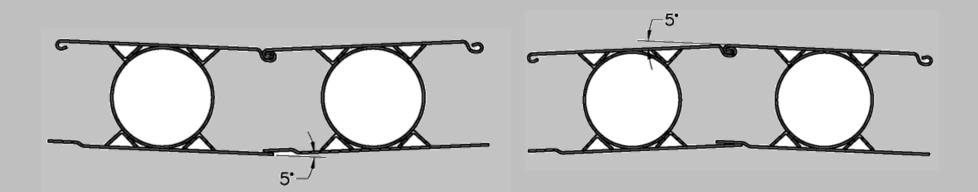
Combi-Wall

Footprint comparison



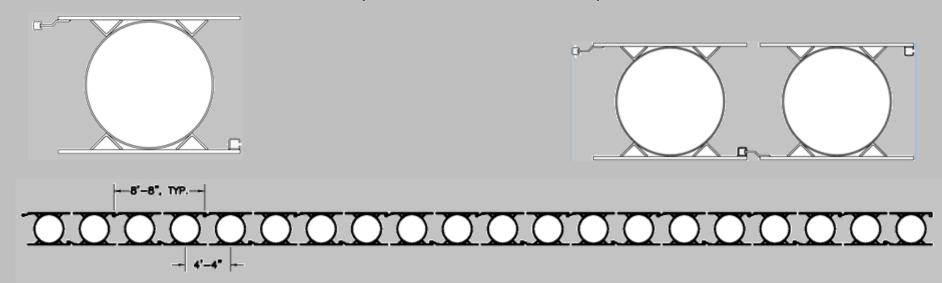
Cold rolled connected FPP





Connected systems

Smaller footprint = less environmental impact





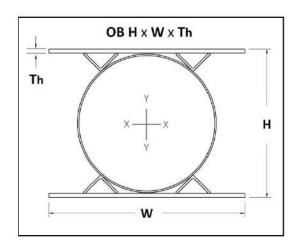


FPP Sections Guide

Standard Nomenclature

In Inches

Flanged Pipe Pile Nominal HEIGHT X Nominal Flange WIDTH x Thickness





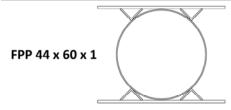
EXAMPLE: **FPP 36** x **48** x **1** at 40 ft.

This is a Flanged Pipe Pile where **the flanges** are; forty (40) foot long 36" height or section depth 48" wide and 1" thick



Standard FPP Section Properties

THEORECTICAL SECTION PROPERTIES







FPP 44 x 60 x 1

 Weight:
 759.4 lbs/lf

 Area Steel:
 223.63 in.²

 Moment of Inertia
 Section Modulus

 $I_x = 82240$ in.4
 $S_x = 3738$ in.3

 $I_y = 58708$ in.4
 $S_y = 1957$ in.3

FPP 36 x 48 x 1

FPP 32 x 42 x 7/8

Weight: 447.1 lbs/lf Area Steel: 131.50 in.²

 Moment of Inertia
 Section Modulus

 $I_x = 25362 \text{ in.}^4$ $S_x = 1598 \text{ in.}^3$
 $I_y = 17270 \text{ in.}^4$ $S_y = 822 \text{ in.}^3$



FPP 26 x 32 x 5/8

FPP 17 x 20 x 5/8

FPP 26 x 32 x 5/8

Weight: 279.4 lbs/lf Area Steel: 82.27 in.²

| Moment of Inertia | Section Modulus | I_x = 9566 in.4 | S_x = 750 in.3 | I_v = 6347 in.4 | S_v = 397 in.3 |

FPP 17 x 20 x 5/8

Weight: 181.7 lbs/lf Area Steel: 53.30 in.²

 Moment of Inertia
 Section Modulus

 I_x = 2747 in.⁴
 S_x = 318 in.³

 I_y = 1750 in.⁴
 S_y = 175 in.³

NOTE: FPP Sections can be customized to suit any specific application



Summary-

PLEASE REMEMBER

FLANGED PIPE PILE

(FPP)

is an effective NEW TOOL

for your pile driving Toolbox.

www.omegatrestle.com

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Thank You!



Any questions?

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